

**The certification of the absorbed energy  
(30 J nominal) of Charpy V-notch reference test pieces  
for tests at 20 °C and at 0 °C: ERM<sup>®</sup>-FA013bk**

**Certified Reference Material ERM<sup>®</sup>-FA013bk**

European Commission  
Joint Research Centre  
Institute for Reference Materials and Measurements

**Contact information**

Reference materials sales  
Retieseweg 111  
B-2440 Geel, Belgium  
E-mail: [jrc-irmm-rm-sales@ec.europa.eu](mailto:jrc-irmm-rm-sales@ec.europa.eu)  
Tel.: +32 (0)14 571 705  
Fax: +32 (0)14 590 406

<http://irmm.jrc.ec.europa.eu/>  
<http://www.jrc.ec.europa.eu/>

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## **CERTIFICATION REPORT**

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tests at 20 °C and at 0 °C: ERM<sup>®</sup>-FA013bk**

**Certified Reference Material ERM<sup>®</sup>-FA013bk**

**A. Lamberty, A. Dean, G. Roebben**

European Commission, Joint Research Centre  
Institute for Reference Materials and Measurements (IRMM)  
Geel, Belgium

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## Summary

This certification report describes the processing and characterisation of ERM<sup>®</sup>-FA013bk, a batch of Charpy V-notch certified reference test pieces certified for the absorbed energy (*KV*) for tests at 20 °C and at 0 °C. Sets of five of these test pieces are used for the verification of pendulum impact test machines according to ISO 148-2 (Metallic materials - Charpy pendulum impact test – Part 2: Verification of testing machines [1]).

The absorbed energy (*KV*) is procedurally defined and refers to the impact energy required to break a V-notched test piece of standardised dimensions, as defined in ISO 148-1 [2]. The certified value of ERM- FA013bk is traceable to the SI, via the SI-traceable certified value of the master batches ERM-FA013ba and ERM-FA013ay, by testing samples of ERM- FA013bk and ERM-FA013ba and ERM-FA013bk and ERM-FA013ay respectively, under repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools. The certified value is valid only for strikers with a 2 mm tip radius. The certified values are valid at  $(20 \pm 2) ^\circ\text{C}$  and  $(0 \pm 2) ^\circ\text{C}$  respectively.

The certified values for *KV* (= energy required to break a V-notched test piece using a pendulum impact test machine) and the associated expanded uncertainties ( $k = 2$  corresponding to a confidence level of about 95 %) calculated for the mean of a set of five test pieces, are:

<b>Steel Charpy V-notch test pieces</b>		
	Certified value <sup>3)</sup> [J]	Uncertainty <sup>4)</sup> [J]
Absorbed energy ( <i>KV</i> ) at 20 °C <sup>1)</sup>	27.8	0.9
Absorbed energy ( <i>KV</i> ) at 0 °C <sup>2)</sup>	26.1	1.1
<p>1) The absorbed energy (<i>KV</i>) is a method defined measurand. <i>KV</i> is the impact energy required to break a V-notched bar of standardised dimensions, as defined in ISO 148-1. The certified value is valid only for strikers with a 2 mm tip radius, and in the temperature range of <math>(20 \pm 2) ^\circ\text{C}</math>.</p> <p>2) The absorbed energy (<i>KV</i>) is a method defined measurand. <i>KV</i> is the impact energy required to break a V-notched bar of standardised dimensions, as defined in ISO 148-1. The certified value is valid only for strikers with a 2 mm tip radius, and in the temperature range of <math>(0 \pm 2) ^\circ\text{C}</math>.</p> <p>3) The certified values of ERM-FA013bk, and the associated uncertainties, are traceable to the International System of Units (SI), via the master batches ERM-FA013ba and ERM-FA013ay respectively, of the same nominal absorbed energy (30 J) by testing samples of ERM-FA013ba and ERM-FA013bk at 20 °C and samples of ERM-FA013ay and ERM-FA013bk at 0 °C, under repeatability conditions on an impact pendulum verified and calibrated with SI-traceable calibrated tools.</p> <p>4) Estimated expanded uncertainty of the mean <i>KV</i> of the 5 specimens (delivered as 1 set), with a coverage factor <math>k = 2</math>, corresponding to a level of confidence of about 95 %, as defined in ISO/IEC Guide 98-3, Guide to the expression of uncertainty in measurement (GUM:1995). The number of degrees of freedom of the certified uncertainty is <math>\nu_{\text{RM}} = 70</math> (20 °C) and 44 (0 °C).</p>		

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## Glossary

AISI	American Iron and Steel Institute
ASTM	American Society for Testing and Materials
BCR	Community Bureau of Reference
CRM	Certified Reference Material
EC	European Commission
ERM <sup>®</sup>	European Reference Material
IMB	International Master Batch
IRMM	Institute for Reference Materials and Measurements
ISO	International Organization for Standardization
JRC	Joint Research Centre
$k$	Coverage factor
$KV$	Absorbed energy = energy required to break a V-notched test piece of defined shape and dimensions when tested with a pendulum impact testing machine
$KV_{CRM}$	Certified $KV$ value of a set of 5 reference test pieces from the Secondary Batch
$KV_{MB}$	Certified $KV$ value of the Master Batch test pieces
LNE	Laboratoire national de métrologie et d'essais
MB	Master Batch
$n_{MB}$	Number of samples of the Master Batch tested during certification of the Secondary Batch
$n_{SB}$	Number of samples of the Secondary Batch tested for certification
$RSD$	Relative standard deviation
$s$	Standard deviation
SB	Secondary Batch
$s_h$	Standard deviation of the results of the samples tested to assess the homogeneity of the Secondary Batch
$s_{MB}$	Standard deviation of the $n_{MB}$ results of the samples of the



	Master Batch tested for the certification of the Secondary Batch
$s_{SB}$	Standard deviation of the $n_{SB}$ results of the samples tested for the characterisation of the Secondary Batch
$u_{CRM}$	Combined standard uncertainty of $KV_{CRM}$
$U_{CRM}$	Expanded uncertainty ( $k = 2$ , confidence level of about 95 %) of $KV_{CRM}$
$u_{char}$	Standard uncertainty of the result of the characterisation tests
$u_{char,rel}$	Relative standard uncertainty of the result of the characterisation tests
$u_h$	Contribution to uncertainty from homogeneity
$u_i$	Value of uncertainty from contribution $i$
$u_{MB}$	Standard uncertainty of $KV_{MB}$
$u_{MB,rel}$	Relative standard uncertainty of $KV_{MB}$
% m/m	Mass fraction
$\bar{X}_{MB}$	Mean $KV$ value of the $n_{MB}$ measurements on samples of the Master Batch tested when characterising the Secondary Batch
$\bar{X}_{SB}$	Mean $KV$ value of the $n_{SB}$ results of the samples tested for the characterisation of the Secondary Batch
$\Delta h$	difference between the height of the centre of gravity of the pendulum prior to release and at the end of the half-swing during which the test sample is broken
$\nu_{RM}$	Effective number of degrees of freedom associated with the uncertainty of the certified value

# 1 Introduction

## 1.1 The Charpy pendulum impact test

The Charpy pendulum impact test is designed to assess the resistance of a material to shock loading. The test, which consists of breaking a notched bar of the test material using a hammer rotating around a fixed horizontal axis, is schematically presented in Figure 1.

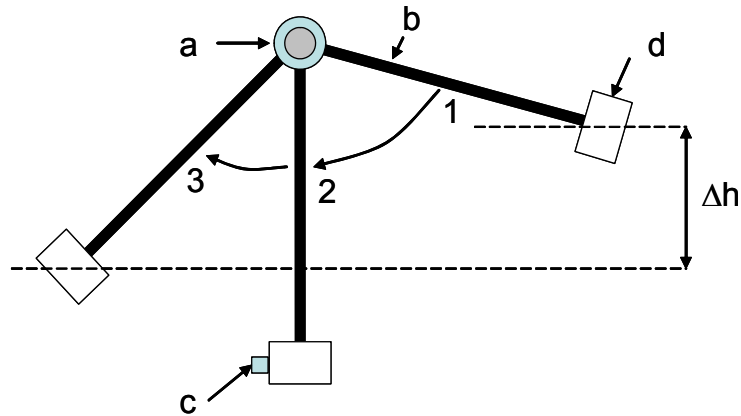


Figure 1: Schematic presentation of the Charpy pendulum impact test, showing a: the horizontal rotation axis of the pendulum, b: the stiff shaft on to which is fixed d: the hammer. The hammer is released from a well-defined height (position 1). When the hammer has reached maximum kinetic energy (shaft in vertical position 2), the hammer strikes c: the test sample, which is positioned on a support and against the pendulum anvils (not shown). The height reached by the hammer after having broken the sample (position 3) is recorded. The difference in height between position 1 and 3 ( $\Delta h$ ) corresponds with a difference in potential energy, and is a measure of the energy required to break the test sample.

The energy absorbed by the test sample is very dependent on the impact pendulum construction and its dynamic behaviour. Methods to verify the performance of an impact pendulum require the use of reference test pieces as described in ISO and other international standards [1, 3]. The reference test pieces dealt with in this report comply with a V-notched test piece shape of well-defined geometry [1], schematically shown in Figure 2.

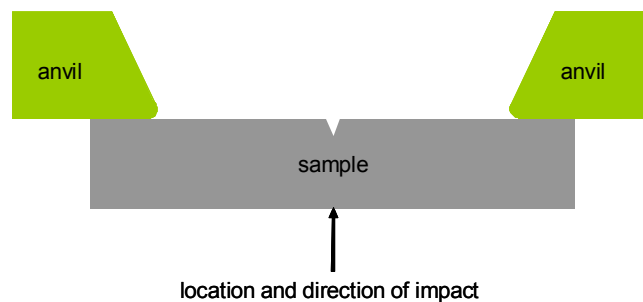


Figure 2: Schematic drawing of a V-notched Charpy test piece (top-view), indicating the place and direction of impact.

## 1.2 The certification concept of Master Batch and Secondary Batch

### 1.2.1 Difference between Master and Secondary Batches

The BCR reports by Marchandise et al. [4] and Varma [5] provide details of the certification of BCR “Master Batches” (MB) of Charpy V-notch certified reference test pieces. The certified value of a Master Batch is obtained using an international laboratory intercomparison.

This report describes the production of a “Secondary Batch” (SB) of Charpy V-notch certified reference test pieces at the Institute for Reference Materials and Measurements (IRMM) of the European Commission's (EC) Joint Research Centre (JRC). The work was performed in accordance with procedures described in the BCR reports [4] and [5]. The certification of a SB is based on the comparison of a set of SB test pieces with a set of test pieces from the corresponding MB under repeatability conditions on a single pendulum.

The BCR reports [4] and [5] were published in 1991 and 1999, respectively. Since 2000, the calculation of the certified value and the estimation of its uncertainty have been updated to an approach compliant with the ISO/IEC Guide to the Expression of Uncertainty in Measurement [6]. This revised approach was developed and presented by Ingelbrecht et al. [7, 8], and is summarised below.

### 1.2.2 Certification of a Secondary Batch of Charpy V-notch test pieces

The certified absorbed energy of a SB of Charpy V-notch reference test pieces ( $KV_{CRM}$ ) is calculated from the mean  $KV$ -value of a set of SB-samples ( $\bar{X}_{SB}$ ) tested on a single pendulum. This value  $\bar{X}_{SB}$  has to be corrected for the bias of this particular pendulum. The bias of the pendulum at the moment of testing the samples of the SB, is estimated by comparing the mean  $KV$ -value of a number of samples of the MB ( $\bar{X}_{MB}$ ), tested together with the SB samples under repeatability conditions, with the certified value of the MB ( $KV_{MB}$ ).  $KV_{CRM}$  is then calculated as follows [8]:

$$KV_{CRM} = \left[ \frac{KV_{MB}}{\bar{X}_{MB}} \cdot \bar{X}_{SB} \right] \quad \text{Eq. 1}$$

For this approach to be reliable, the pendulum used for the tests on MB and SB in repeatability conditions, must be well performing. In other words, the ratio  $\frac{KV_{MB}}{\bar{X}_{MB}}$  must be close to 1. IRMM allows a difference of 5 % ( $KV_{MB} \geq 40$  J) or 2 J ( $KV_{MB} < 40$  J) between  $KV_{MB}$  and  $\bar{X}_{MB}$ , corresponding with the level of bias allowed for reference pendulums specified in ISO 148-3 [9].

Also, for reasons of commutability, a comparable response of the pendulum to the MB and SB samples is required. This is the reason why MB and SB samples are made from nominally the same steel. Moreover, it is checked that the ratio  $\frac{KV_{CRM}}{KV_{MB}}$  is close to 1. IRMM now allows a difference of 20 % ( $KV_{MB} \geq$

40 J) or 8 J ( $KV_{MB} < 40$  J) between  $KV_{CRM}$  and  $KV_{MB}$  to ensure that the MB and SB samples have a comparable interaction with the pendulum.

### 1.2.3 Uncertainty of the certified value of a Secondary Batch of Charpy V-notch test pieces

The uncertainty of the certified value of the SB is a combination of the uncertainties of the right-hand side factors in Eq. 1. It is clear that the MB-SB approach necessarily results in a larger uncertainty of the certified value of SB in comparison with the MB. The additional uncertainty depends on the uncertainty of the ratio  $\bar{X}_{MB}/\bar{X}_{SB}$ . The full measurement uncertainty of the values  $\bar{X}_{MB}$  and  $\bar{X}_{SB}$  is relatively large. However, when all conditions mentioned above (repeatability conditions, pendulum performance, and commutability between Secondary and Master Batch) are fulfilled, then the uncertainties of the values  $\bar{X}_{MB}$  and  $\bar{X}_{SB}$  have several contributions in common, in particular the uncertainty due to the bias of the pendulum. These shared uncertainty components do not contribute to the uncertainty of the ratio  $\bar{X}_{MB}/\bar{X}_{SB}$ , and only the standard deviations of the SB and MB results in the MB-SB comparison test need to be taken into account (see also Section 6.3). Thus, the MB-SB comparison approach can produce a value for the uncertainty of  $KV_{CRM}$  that is sufficiently small to meet the requirements of the intended use of the certified reference material (CRM).

## 2 Participants

The processing of the SB (ERM-FA013bk) test pieces was carried out by the Laboratoire national de métrologie et d'essais (LNE), Trappes (FR), using steel bars produced at Aubert&Duval (FR). The MB samples (ERM-FA013ba) used in the characterisation of the SB were provided by IRMM, Geel (BE). The homogeneity of the SB was evaluated based on data obtained at LNE using a pendulum verified according to the criteria imposed by ISO 148-2 [1]. Characterisation of the SB was carried out at IRMM using a pendulum verified according to the criteria imposed by ISO 148-2 [1]. The tests performed were within the scope of an ISO/IEC 17025 accreditation (BELAC 268-Test). Data evaluation was performed at IRMM. The certification project performed was within the scope of an ISO Guide 34 accreditation (BELAC 268-RM).

## 3 Processing

The ERM- FA013bk test pieces were prepared from AISI 4340 steel. The steel was cast and rolled into bars at Aubert&Duval (see Section 3.1). Production of the test pieces from these bars was performed under the supervision of LNE (see Sections 3.2, 3.3, 3.4 and 3.5).

### 3.1 Processing of hot-rolled bars

The base material consisted of AISI 4340 steel produced at Aubert&Duval. To limit the amount of impurities potentially affecting the homogeneity of the fracture resistance, the following compositional tolerances were imposed on the selected steel batch: Mn 0.7 – 0.8, Mo 0.23 - 0.28, Ni 1.7 – 1.85, P < 0.01, Si 0.2 – 0.35, S < 0.008 (in % m/m), which is stricter than generally allowed

for AISI 4340. The ingot was hot rolled, resulting in bars that were 4 m long and with a squared cross-Section of 11.5 x 11.5 mm. For the ERM-FA013bk batch, steel was used from ingot number HM157001. A full description of the processing and quality check of the steel bars was provided by Aubert&Duval and LNE.

### **3.2 Heat treatment of hot-rolled bars**

The heat treatment of the hot-rolled bars was performed at Aubert&Duval. 15 bars were heat-treated together. Bars were placed onto rollers which slowly move the bars back and forth inside the furnace during the heat treatment to increase the homogeneity of the resulting microstructure. The first heat treatment was an austenisation treatment performed in a furnace of 'class 10 °C' <sup>1</sup> at 850 °C for 30 min. From this furnace, the bars were quenched into oil at 40 °C. After the oil-quench, the samples were annealed in a furnace of 'class 5 °C' at 350 °C for 120 min for ERM- FA013bk. After this annealing treatment, the samples were cooled down in air.

### **3.3 Machining of Charpy test pieces**

After heat treatment, a limited number of samples (5) were machined for a preliminary check of the obtained energy level. Results indicated an average KV-level (26.0 J for ERM-FA013bk) which is within the desired energy range (22.5 J to 27.5 J).

The samples were machined to dimensional tolerances imposed in ISO 148-3 [9]. The batch code (indicating the nominal energy level and the letter code assigned to the batch) and the individual sample code (indicating the bar and the sequence in the bar from which the sample originates) were engraved twice on one long face of each sample, on both sides of the notch, for fully traceable sample coding also after fracture. The V-notch was introduced using an electro-erosion tool.

### **3.4 Quality control**

When all samples from the batch were fully machined, a selection of 25 samples was made. The dimensions of the 25 samples were checked on June 19, 2012 against the criteria specified in ISO 148-3 [9] (length  $55.0^{+0.00}_{-0.30}$  mm, height  $10.00 \pm 0.06$  mm, width  $10.00 \pm 0.07$  mm, notch angle  $45 \pm 1^\circ$ , height remaining at notch root  $8.00 \pm 0.06$  mm, radius at notch root  $0.250 \pm 0.025$  mm, distance between the plane of symmetry of the notch and the longitudinal axis of the test piece  $27.5 \pm 0.2$  mm). All samples were within the ranges specified in ISO 148-3 [9].

For each batch 25 samples checked for geometrical compliance were impact tested on the Tinius Olsen, model 74 impact (serial number 126 385)

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<sup>1</sup> In a furnace of 'class x °C', the variation of the temperature is smaller than x °C. The furnaces used have 10 heating zones. Each zone has 3 controlling thermocouples and 3 measurement thermocouples. These are regularly calibrated. When one faulty thermocouple is detected, it is replaced by a thermocouple produced with wire from the same roll. When a roll is exhausted, all thermocouples are replaced with new ones.

pendulum - which is one of the French reference pendulums - at LNE on June 19, 2012. The results are reported in an LNE certificate.

The average  $KV$  of the 25 samples was 29.10 J, which is sufficiently close to the desired energy range (22.5 – 27.5 J). The standard deviation of the test results was  $s = 0.55$  J,  $RSD = 1.9$  %. The variation was checked again during the characterisation tests at IRMM (see Section 6).

### 3.5 Packaging and storage

Finally, the samples were cleaned and packed in sets of 5, in oil-filled and closed plastic bags. These oil-filled bags, together with a label, again were packed in a sealed plastic bag, and shipped to IRMM. After arrival (July 12, 2012) the 1390 samples (or 278 sets) of ERM-FA013bk were registered and stored at room temperature ( $18\text{ }^{\circ}\text{C} \pm 5\text{ }^{\circ}\text{C}$ ), pending distribution.

## 4 Homogeneity

The test pieces are sampled from the SBs, which are sufficiently, but not perfectly, homogeneous. Therefore, an appropriate homogeneity contribution  $u_h$  to the uncertainty of the certified value is required.  $u_h$  is related to  $s_h$ , the standard deviation between the samples in the SB (*sample-to-sample heterogeneity*), but also depends on the number of samples over which the  $KV$ -value is averaged. ISO 148-2 [1] specify that the pendulum verification must be performed using 5 test pieces, which is why a CRM-unit consists of a set of 5 test pieces. The appropriate uncertainty contribution must be an estimate of the *set-to-set heterogeneity*, which in the case of a set of 5 test

pieces can be calculated as  $u_h = \frac{s_h}{\sqrt{5}}$ .

Here,  $u_h$  is estimated from  $s_h$ , the standard deviation of results obtained at LNE on June 19, 2012 ( $s_h = 0.55$  J). This leads to  $u_h = \frac{s_h}{\sqrt{5}} = 0.25$  J (0.85 %).

As is required for a homogeneity test, the samples were randomly selected from the whole batch. The number of samples tested (25) is sufficiently large to reflect the homogeneity of the full SB (1390 samples). It can be noted that  $u_h$  is probably a slight overestimation, since it contains also the repeatability of the instrument. However, the latter cannot be separated or separately measured.

## 5 Stability

The stability of the absorbed energy of Charpy V-notch certified reference test pieces was first systematically investigated for samples of nominally 120 J by Pauwels et al., who did not observe measurable changes of absorbed energy [10]. Additional evidence for the stability of the reference test pieces produced from AISI 4340 steel of lower energy levels (nominally 15 J, 30 J and 100 J) has been obtained during the International Master Batch (IMB) project [11]. In the IMB-project, the stability of the certified test pieces was judged from the change of the mean of means of the absorbed energy obtained on 7 reference pendulums over a three year period. None of the three regression

slopes for the tested energy levels was statistically significant at the 0.05 significance level. Given the large sample-to-sample heterogeneity and the limited number of samples (5) in a CRM unit, the uncertainty contribution from instability is considered to be insignificant in comparison to that of homogeneity.

The main reason for the microstructural stability of the certified reference test pieces is the annealing treatment to which the samples were subjected after the austenisation treatment. Annealing is performed at temperatures where the equilibrium phases are the same as the (meta-)stable phases at ambient temperature ( $\alpha$ -Fe and Fe<sub>3</sub>C). The only driving force for instability stems from the difference in solubility of interstitial elements in the  $\alpha$ -Fe matrix, between annealing and ambient temperature. Relaxation of residual (micro-)stress by short-range diffusion or the additional formation or growth of precipitates during the shelf-life of the certified reference test pieces is expected to proceed but slowly.

In the meanwhile efforts are spent to better establish the stability of the certified values of batches of Charpy CRMs. Until such further notice, it is decided to specify a limited shelf-life. A period of 10 years is chosen, counting from the date of the characterisation tests on the SB. Since batch ERM-FA013bk was characterised in August 2012, the certificate is valid until August 2022.

## **6 Characterisation**

### **6.1 Characterisation tests**

Characterisation tests were made at 20 and at 0 °C.

For the tests at 20 °C 30 samples from the SB ERM-FA013bk (sets 1, 20, 92, 115, 197 and 270) were tested under conditions of repeatability with 25 samples from MB ERM-FA013ba (sets 16, 76, 122, 214 and 259). For the tests at 0 °C 30 samples from the SB ERM-FA013bk (sets 2, 43, 107, 179, 198 and 276) were tested under conditions of repeatability with 25 samples from MB ERM-FA013ay (sets 4, 78, 135, 189 and 245). The measurements were done using the Instron Wolpert PW 30 (serial number 7300 H1527) machine of IRMM, an impact pendulum yearly verified according to procedures described in ISO 148-2 [1]. Tests at 20 °C were performed on August 17, 2012 and tests at 0 °C on August 22, 2012 (laboratory temperature  $20 \pm 1$  °C), in accordance with ISO 148-1 [2]. The measurement sequence for both temperatures was: SB-MB-SB-MB-SB-MB-SB-MB-SB-MB-SB. The measured absorbed energy values were corrected for friction and windage losses.

7 of the 30 samples of ERM-FA013bk and 3 of the 25 samples of ERM-FA013ba tested at 20 °C gave excessively high absorbed energy values. None of the 30 samples of ERM-FA013bk and of the 25 samples of ERM-FA013ay tested at 0 °C gave excessively high absorbed energy values. One result on FA013bk had however to be eliminated because of misalignment.

Inspection of the broken samples reveals the same type of damage as observed on previous FA013 batches. After testing, all Charpy samples show 'first-strike' marks: these are the marks caused by the interaction between sample and anvils during the first and intended hammer impact. Upon fracture, the broken half samples loose contact with hammer and anvils and follow one of a variety of possible trajectories, away from the pendulum, depending on the properties of both pendulum and test material. Some samples show 'second-strike' marks. These are marks caused by a second impact of the already broken half samples back onto the anvils. This phenomenon has been described by Schmieder et al. [12]. Most of the broken FA013bk, FA013ba and FA013ay samples show second-strike marks. A mere second impact of the broken half samples onto the anvils does not affect the measured KV value, since it does not involve or slow down the swinging pendulum.

For 10 samples (7 of FA013bk and 3 of FA013ba) measured at 20 °C, a significant post-fracture deformation mark on one of the long edges of the notched face of the sample was observed. Systematically, this indent is accompanied by a broader deformation of the diagonally opposite long edge (on the face of the sample opposite the notch). This suggests that the samples, during the second strike onto the anvils, were briefly caught between anvil and a part of the swinging pendulum. This induces erroneously high measured absorbed energy values. For this technical reason, these data were eliminated from the evaluation. All other data were accepted. An analysis of the normality of the distribution of remaining KV values did not indicate a skewed distribution towards higher or lower absorbed energy values.

The same parasitic energy absorbing phenomenon occurred also for some but not all of the other batches which were prepared previously. Also, the phenomenon did not occur during the pre-acceptance tests at LNE. Furthermore, the FA013ba batch was tested on 12 pendulums during a laboratory intercomparison, revealing that post-fracture energy absorption occurs only for a minority of the pendulums involved (2 out of 12).

The above observations indicate that excessive post-fracture energy absorption affecting the measured KV values can occur, but only for a limited number of combinations of pendulum and material. In each case, excessively high measured values are easily related to large post-fracture deformation marks on the broken samples. Users of ERM-FA013bk certified reference materials encountering outlier values that can be related to post-fracture indentation marks on the broken samples are requested to eliminate the corresponding data from the analysis of their results.

The comparison of the indirect verification results with the certified value and uncertainty is based on the mean of the 5 measured KV values, because this is the sample size for which the uncertainty of the certified value has been calculated. If outlier values have to be eliminated because of post-fracture indentation, the corresponding expanded uncertainty is for ERM-FA013bk with  $n = 4$  remaining results  $U = 0.9$  J, for  $n = 3$  remaining results  $U = 1.0$  J.



This jamming effect occurs to a lesser extent at 0 °C. For these measurement series none of the samples showed significant post-fracture marks. One result was eliminated because of misalignment.

The accepted data obtained on individual test pieces are shown in Figures 3a and 3b and Annexes 1a and 1b. The results of the measurements are summarised in Tables 1a and 1b.

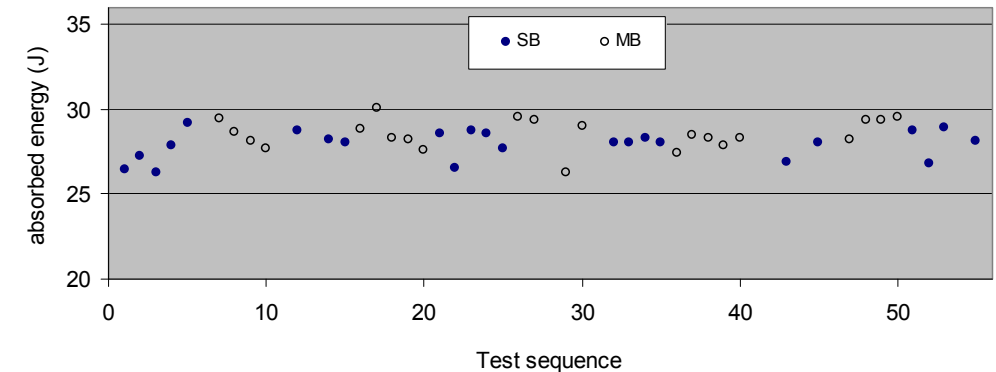


Figure 3a: Absorbed energy values of 22 test pieces of ERM-FA013ba obtained at 20 °C, compared with 23 test pieces of ERM-FA013bk; data are displayed in the actual test sequence

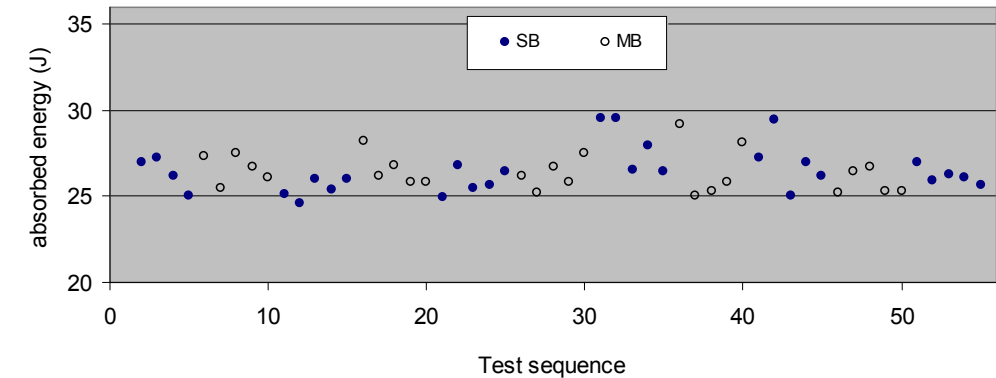


Figure 3b: Absorbed energy values of 25 test pieces of ERM-FA013ay obtained at 0 °C, compared with 29 test pieces of ERM-FA013bk; data are displayed in the actual test sequence

Table 1a: Characterisation measurements of Batch ERM-FA013bk (20 °C)

	Number of test pieces $n_{MB}, n_{SB}$	Mean value $\bar{X}_{MB}, \bar{X}_{SB}$ [J]	Standard deviation $s_{MB}, s_{SB}$ [J]	Relative standard deviation $RSD_{SB}, RSD_{MB}$ [%]
<b>ERM®-FA013ba (MB)</b>	22	28.54	0.89	3.12
<b>ERM®-FA013bk (SB)</b>	23	27.93	0.84	3.01

Table 1b: Characterisation measurements of Batch ERM-FA013bk (0 °C)

	Number of test pieces $n_{MB}, n_{SB}$	Mean value $\bar{X}_{MB}, \bar{X}_{SB}$ [J]	Standard deviation $s_{MB}, s_{SB}$ [J]	Relative standard deviation $RSD_{SB}, RSD_{MB}$ [%]
<b>ERM®-FA013ay (MB)</b>	25	26.40	1.09	4.13
<b>ERM®-FA013bk (SB)</b>	29	26.48	1.31	4.95

The SB-results meet the ISO 148-3 acceptance criteria for a batch of reference materials ( $s_{SB} < 2$  J for  $KV_{SB} < 40$  J).

## 6.2 Data from Master Batch ERM-FA013ba (20 °C) and ERM-FA013ay (0 °C)

To calculate  $KV_{CRM}$  for ERM-FA013bk one needs  $KV_{MB}$  of the MB used, i.e. ERM-FA013ba and ERM-FA013ay respectively. Tables 2a and 2 b show the main MB-data, taken from the Certificate of Analysis of ERM-FA013ba and ERM-FA013ay respectively (Annexes 2a and 2b).

Table 2a: Data from the certification of Master Batch ERM-FA013ba

	<b>Certified absorbed energy of Master Batch</b>	<b>Standard uncertainty of <math>KV_{MB}</math></b>	<b>Relative standard uncertainty of <math>KV_{MB}</math></b>
	$KV_{MB}$ (J)	$u_{MB}$ (J)	$u_{MB,rel}$ (%)
<b>ERM®- FA013ba</b>	28.46	0.23	0.81

Table 2b: Data from the certification of Master Batch ERM-FA013ay

	<b>Certified absorbed energy of Master Batch</b>	<b>Standard uncertainty of <math>KV_{MB}</math></b>	<b>Relative standard uncertainty of <math>KV_{MB}</math></b>
	$KV_{MB}$ (J)	$u_{MB}$ (J)	$u_{MB,rel}$ (%)
<b>ERM®- FA013ay</b>	26.06	0.35	1.34

## 6.3 Calculation of $KV_{CRM}$ and of $u_{char}$

From the data in Tables 1a, 1b, 2a and 2b, and using Eq. 1,  $KV_{CRM}$  can be calculated:

$$KV_{CRM} = 27.8 \text{ J (20 °C)}$$

$$KV_{CRM} = 26.1 \text{ J (0 °C)}$$

Rounding is done in accordance with uncertainty; see Table 4a and 4b). The uncertainty associated with the characterisation of the SB,  $u_{char}$ , is assessed as in Eq. 2 [8], which sums the relative uncertainties of the three factors in Eq. 1:

$$u_{char} = KV_{CRM} \sqrt{\frac{u_{MB}^2}{KV_{MB}^2} + \frac{s_{SB}^2}{n_{SB} \cdot \bar{X}_{SB}^2} + \frac{s_{MB}^2}{n_{MB} \cdot \bar{X}_{MB}^2}} \quad \text{Eq. 2}$$

$\bar{X}_{SB}$  and  $\bar{X}_{MB}$  were obtained under repeatability conditions. Therefore, the uncertainty of the ratio  $\bar{X}_{SB} / \bar{X}_{MB}$  is not affected by the contributions from reproducibility and bias of the pendulum used to compare MB and SB. Tables

3a and 3b summarise the input quantities of the  $u_{\text{char}}$  uncertainty budget, their respective statistical properties, and shows how they were combined.

The effective number of degrees of freedom ( $\nu_{\text{eff}}$ ) for  $u_{\text{char}}$  is obtained using the Welch-Satterthwaite equation from the combined uncertainty ( $u_c$ ) and the individual uncertainty contributions ( $u_i$ ) and their respective degrees of freedom ( $\nu_i$ ) (Eq. 3) [6].

$$\nu_{\text{eff}} = \frac{u_c^4}{\sum_{i=1}^N \frac{u_i^4}{\nu_i}} \quad \text{Eq. 3}$$

*Table 3a: Uncertainty budget for  $u_{\text{char}}$  for ERM-FA013bk (20 °C)*

FA013bk	source of uncertainty	measured value (J)	standard uncertainty (J)	probability distribution	divisor	sensitivity coefficient	relative uncertainty (%)	degrees of freedom
$KV_{\text{MB}}$	Certification of MB	28.46	0.23	normal	1	1	0.81	14
$\bar{X}_{\text{SB}}$	comparison of SB and MB in repeatability conditions	27.93	0.17	normal	1	1	0.62	22
$\bar{X}_{\text{MB}}$		28.54	0.19	normal	1	1	0.66	21
$u_{\text{char,rel}}$ (%)							1.22	47
$u_{\text{char}}$ (J)							0.34	

*Table 3b: Uncertainty budget for  $u_{\text{char}}$  for ERM-FA013bk (0 °C)*

FA013bk	source of uncertainty	measured value (J)	standard uncertainty (J)	probability distribution	divisor	sensitivity coefficient	relative uncertainty (%)	degrees of freedom
$KV_{\text{MB}}$	Certification of MB	26.06	0.35	normal	1	1	1.34	11
$\bar{X}_{\text{SB}}$	comparison of SB and MB in repeatability conditions	26.48	0.24	normal	1	1	0.92	28
$\bar{X}_{\text{MB}}$		26.40	0.22	normal	1	1	0.82	24
$u_{\text{char,rel}}$ (%)							1.83	32
$u_{\text{char}}$ (J)							0.48	

## 7 Value assignment

### 7.1 Certified value, combined and expanded uncertainty

As shown in 6.3,  $KV_{CRM} = 27.8$  J at 20 °C and 26.1 J at 0 °C. The uncertainty of the certified value is obtained by combining the contributions from the characterisation study,  $u_{char}$ , and from the homogeneity assessment,  $u_h$ , as is summarized in the following uncertainty budget (Tables 4a and 4b).

The relevant number of degrees of freedom calculated using the Welch-Satterthwaite equation [6], is sufficiently large ( $\nu_{RM} = 70$  and 44 respectively) to justify the use of a coverage factor  $k = 2$  to expand the confidence level to about 95 %. The obtained expanded uncertainty provides justification for the SB-MB approach followed:  $U_{CRM}$  is sufficiently smaller ( $U_{CRM} = 0.9$  J and 1.1 J respectively) than the verification criterion of 4 J for industrial pendulums [1] or even 2 J for reference pendulums [9].

Table 4a: Uncertainty budget of  $KV_{CRM}$  for ERM-FA013bk (20 °C)

FA013bk	source of uncertainty	relative value $u_i$ (%)		degrees of freedom
$u_{char}$	characterisation of SB	1.22		47
$u_h$	homogeneity of SB	0.86		24
Combined standard uncertainty, $u_{CRM}$ (%)		1.49	70	
Combined standard uncertainty, $u_{CRM}$ (J)		0.42		
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (%)		3.0		
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (J)		0.9		

Table 4b: Uncertainty budget of  $KV_{CRM}$  for ERM-FA013bk (0 °C)

FA013bk	source of uncertainty	relative value $u_i$ (%)		degrees of freedom
$u_{char}$	characterisation of SB	1.83		32
$u_h$	homogeneity of SB	0.86		24
Combined standard uncertainty, $u_{CRM}$ (%)		2.02	44	
Combined standard uncertainty, $u_{CRM}$ (J)		0.53		
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (%)		4.1		
Expanded Uncertainty, $k = 2$ , $U_{CRM}$ (J)		1.1		

## **8 Metrological traceability and commutability**

The certified property is defined by the Charpy pendulum impact test procedure described in ISO 148-1 [2].

The certified values of the MB ERM-FA013ba and ERM-FA013ay are traceable to the SI, since they were obtained using an interlaboratory comparison, involving a representative selection of qualified laboratories performing the tests in accordance with the standard procedures and using instruments verified and calibrated with SI-traceable calibration tools.

The certified value of ERM-FA013bk is made traceable to the SI-traceable certified value of the MB by testing SB and MB samples in repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools. Therefore, the certified values of ERM-FA013bk are traceable to the International System of Units (SI) via the corresponding Master Batches ERM-FA013ba and ERM-FA013ay of the same nominal absorbed energy (30 J). Absorbed energy *KV* is a method-specific value, and can only be obtained by following the procedures specified in ISO 148-1 [2].

The intended use of the certified reference test pieces is the verification of Charpy impact pendulums. During the certification of the MB, different pendulums were used, each equipped with an ISO-type striker of 2 mm tip radius. Until further notice, the certified values are not to be used when the test pieces are broken with an ASTM-type striker of 8 mm tip radius [10].

## **9 Instructions for use**

### **9.1 Safety information**

Precautions need to be taken to avoid injury of the operator by broken specimens when operating the Charpy impact pendulum.

### **9.2 Intended use**

Samples of ERM-FA013bk correspond to the 'certified reference test pieces' as defined in ISO 148-3 [9]. Sets of five of these certified reference test pieces are intended for the indirect verification of impact testing machines with a striker of 2 mm tip radius according to procedures described in detail in ISO 148-2 [1].

The indirect verification provides an assessment of the bias of the user's Charpy pendulum impact machine. This bias assessment can be used in the calculation of the measurement uncertainty of Charpy tests on the pendulum after indirect verification. Such uncertainty calculation requires the certified value, the associated uncertainty, and in some cases also the degrees of freedom of the uncertainty, all given on page 1 of the certificate.

### **9.3 Sample preparation**

Special attention is drawn to the cleaning of the specimens prior to the tests. It is mandatory to remove the oil from the sample surface prior to testing, without damaging the edges of the sample. Between the moment of removing the protective oil layer and the actual test, corrosion can occur. This must be avoided by limiting this period of time, while keeping the sample clean.

The following procedure is considered a good practice.

1. First use absorbent cleaning-tissue to remove the excess oil. Pay particular attention to the notch of the sample, but do not use hard (e.g. steel) brushes to remove the oil from the notch.
2. Submerge the samples in ethanol for about 5 min. Use of ultrasonication is encouraged, but only if the edges of the samples are prevented from rubbing against each other. To reduce the consumption of solvent, it is allowed to make a first cleaning step with detergent, immediately prior to the solvent step.
3. Once samples are removed from the solvent, only manipulate the samples wearing clean gloves. This is to prevent development of corrosion between the time of cleaning and the actual test.
- 4a. Before testing at 20 °C, bring the specimens to the test temperature ( $20 \pm 2$ ) °C. To assure thermal equilibrium is reached, move the specimens to the test laboratory at least 3 h before the tests.
- 4b. Before testing at 0 °C, bring the specimens to the test temperature ( $0 \pm 2$  °C). To assure thermal equilibrium, the specimens shall be at least 10 minutes in a liquid cooling medium or at least 30 minutes in a gaseous cooling medium, the temperature of which is measured and monitored. The test piece shall be broken within 5 seconds of the time of removal from the cooling medium.

### **9.4 Pendulum impact tests**

After cleaning, the 5 samples constituting a CRM-unit need to be broken with a pendulum impact test machine in accordance with ISO 148-1 [2] standards. Prior to the tests, the anvils must be cleaned. It must be noted that Charpy test pieces sometimes leave debris on the Charpy pendulum anvils. Therefore, the anvils must be checked regularly and if debris is found, it must be removed. The uncertainty of the certified value applies to the mean of the 5 KV-values.

### **9.5 Storage**

Specimens should be kept at room temperature ( $18 \pm 5$ ) °C in their original packing until used. The European Commission cannot be held responsible for changes that happen during storage of the material at the customer's premises, especially of opened samples.

## **Acknowledgements**

The authors wish to thank M. Ricci, A. Held, R. Koeber, and H. Emons (all IRMM) for reviewing of the certification report.



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## Annex 1a

Results of characterisation measurements at 20 °C of ERM-FA013bk as measured according to ISO 148-1 at IRMM, August 17, 2012.

	Master Batch ERM-FA013ba	Secondary Batch ERM-FA013bk
	<i>KV (J)</i>	<i>KV (J)</i>
1	29.44	26.45
2	28.66	27.29
3	28.13	26.26
4	27.69	27.88
5	28.86	29.18
6	30.04	28.73
7	28.33	28.20
8	28.20	28.07
9	27.56	28.60
10	29.51	26.53
11	29.38	28.73
12	26.27	28.60
13	28.99	27.69
14	27.42	28.07
15	28.46	28.07
16	28.27	28.33
17	27.88	28.07
18	28.33	26.91
19	28.20	28.07
20	29.38	28.73
21	29.38	26.85
22	29.58	28.93
23		28.14
<b>Mean (J)</b>	<b>28.54</b>	<b>27.93</b>
<b>Standard deviation (J)</b>	<b>0.89</b>	<b>0.83</b>
<b>RSD (%)</b>	<b>3.12</b>	<b>2.99</b>

## Annex 1b

Results of characterisation measurements at 0 °C of ERM-FA013bk as measured according to ISO 148-1 at IRMM, August 22, 2012.

	Master Batch ERM-FA013ay	Secondary Batch ERM-FA013bk
	<i>KV (J)</i>	<i>KV (J)</i>
1	27.35	26.96
2	25.44	27.22
3	27.48	26.20
4	26.70	25.06
5	26.07	25.12
6	28.25	24.61
7	26.20	26.00
8	26.83	25.37
9	25.81	26.00
10	25.81	24.93
11	26.18	26.83
12	25.24	25.44
13	26.76	25.69
14	25.87	26.45
15	27.48	29.56
16	29.17	29.56
17	25.06	26.58
18	25.31	27.99
19	25.81	26.45
20	28.12	27.22
21	25.18	29.43
22	26.45	25.06
23	26.70	26.96
24	25.31	26.20
25	25.31	26.96
26		25.94
27		26.32
28		26.07
29		25.69
30		
<b>Mean (J)</b>	<b>26.40</b>	<b>26.48</b>
<b>Standard deviation (J)</b>	<b>1.09</b>	<b>1.31</b>
<b>RSD (%)</b>	<b>4.12</b>	<b>4.96</b>



# CERTIFICATE OF ANALYSIS

ERM®- FA013ba

STEEL		
	Impact toughness	
	Certified value <sup>2)</sup> [J]	Uncertainty <sup>3)</sup> [J]
Absorbed energy (KV) <sup>1)</sup>	28.46	0.23
<p>1) The absorbed energy (KV) is procedurally defined and refers to the impact energy required to break a V-notched bar of standardised dimensions, as defined in EN 10045-1 and ISO 148-1.</p> <p>2) The certified value is estimated as the mean of means of absorbed energies measured at 15 laboratories. At each laboratory, 20 test pieces were broken. The instruments used by these laboratories are regularly verified with equipment that is calibrated in a manner that is traceable to the International System of Units (SI). Therefore, the certified value is traceable to the International System of Units (SI).</p> <p>3) Standard uncertainty <math>u</math> of the certified mean absorbed energy of batch ERM-FA013ba, estimated as the standard deviation of the mean of the 15 laboratory mean values, corresponding with a confidence level of about 68 %.</p>		

This certificate is valid until January 2018.

## NOTE

European Reference Material ERM®-FA013ba was produced and certified under the responsibility of the Institute for Reference Materials and Measurements of the European Commission's Joint Research Centre according to the principles laid down in the technical guidelines of the European Reference Materials® co-operation agreement between BAM-IRMM-LGC. Information on these guidelines is available on the internet (<http://www.erm-crm.org>).

Accepted as an ERM®, Geel, January 2009.

Signed: \_\_\_\_\_

Prof. Dr. Hendrik Emons  
European Commission  
Joint Research Centre  
Institute for Reference Materials and Measurements  
Retieseweg 111  
B-2440 Geel, Belgium



Registration No. 268-TEST  
ISO Guide 34 for the  
production of reference materials

All following pages are an integral part of the certificate.

Page 1 of 3

## DESCRIPTION OF THE SAMPLE

A unit consists of five Charpy V-notch test pieces, which are rectangular steel bars of nominal dimensions 55 mm x 10 mm x 10 mm, with one V-notch, accurately machined to tolerances imposed in EN 10045-2 and ISO 148-3. The five specimens are packed together in a plastic bag filled with oil to prevent oxidation.

## ANALYTICAL METHOD USED FOR CERTIFICATION

Charpy pendulum impact tests in accordance with EN 10045-1 and ISO 148-1, using pendulum impact machines with a 2 mm striker tip radius.

## PARTICIPANTS

- Aubert&Duval, Les Ancizes and Gennevilliers (FR)
- Bodycote Materials Testing, Emmen (NL)\* (RvA testen L085)
- Bodycote Materials Testing, Spijkenisse (NL)\* (RvA testen L085)
- Bundesanstalt für Materialforschung und -prüfung (BAM), Abteilung V Werkstofftechnik, Berlin (DE)\* (DAP-PL-2614.16)
- Centro de Apoio Tecnológico a Indústria Metalomecânica (CATIM), Laboratório de Ensaios, Porto (PT)\* (IPAC L009)
- Cogne Acciai Speciali, Aosta (IT)
- Fraunhofer Gesellschaft, Institut für Werkstoffmechanik, Freiburg (DE)
- European Commission Joint Research Centre (JRC), Institute for Reference Materials and Measurements, Geel (BE) (BELAC 268-Test)
- Korea Research Institute of Standards and Science, Strength Evaluation Group, Daejeon, Korea
- Laboratoire National de Métrologie et d'Essais, Charpy Laboratory, Trappes (FR)\* (COFRAC SMH 2-1287)
- National Institute of Standards and Technology (NIST), Materials Reliability Division, Boulder, USA
- SCK-CEN, Labo Reactormaterialenonderzoek, Mol (BE)\* (BELAC 015-Test)
- SIRRIIS, Beproevingslaboratorium Gent, Zwijnaarde (BE)\* (BELAC 232-Test)
- U.S. Steel Košice, Labortest, Košice (SK)\* (SNAS 026/S012)
- Universität Stuttgart, Materialprüfungsanstalt, Stuttgart (DE)\* (DAP-PL-2907.02)
- VTT, Espoo (FI)

\* Measurements within the scope of accreditation to ISO 17025.

## SAFETY INFORMATION

Precautions need to be taken to avoid injury of the operator by broken specimens when operating the Charpy impact pendulum.

## INSTRUCTIONS FOR USE

Samples of ERM-FA013ba correspond with the '(certified) BCR test pieces' as referred to in EN 10045-2 (Method for the verification of impact testing machines), as well as with the 'certified reference test pieces' as defined in ISO 148-3 (Preparation and characterisation of Charpy V reference test pieces for verification of test machines).

The ERM-FA013ba batch is one of the 'Master Batches'. Master Batch test pieces are not for sale. They are intended solely to traceably certify Secondary Batches of the same nominal absorbed energy (here 30 J). The certified value and its associated uncertainty of the Master Batch are used in the calculation of the certified value and combined and expanded uncertainty of a set of 5 specimens from a Secondary Batch.

When characterising a secondary batch, a number of Master Batch test pieces are broken under repeatability conditions together with a selection of samples from the secondary batch. Special attention is drawn to the cleaning and conditioning of the specimens prior to testing. It is mandatory to remove the oil from the sample surface prior to testing, without damaging the edges of the sample. Between the moment of

removing the protective oil layer and the actual test, corrosion can occur. This must be avoided by limiting this period of time, while keeping the sample clean.

The following cleaning and conditioning procedure is considered to be good practice.

1. First use absorbent cleaning-tissue to remove the excess oil. Pay particular attention to the notch of the sample, but do not use hard (e.g. steel) brushes to remove the oil from the notch.
2. Submerge the samples in technically pure ethanol for about 5 minutes. Use of ultrasonication is encouraged, but only if the edges of the samples are prevented from rubbing against each other. To reduce the consumption of solvent, it is allowed to make a first cleaning step with detergent, immediately prior to the solvent step.
3. Once samples are removed from the solvent, only manipulate the samples wearing clean gloves. This is to prevent development of corrosion between the time of cleaning and the actual test.
4. Before testing, bring the specimens to the test temperature ( $20 \pm 2$  °C). To assure thermal equilibrium is reached, move the specimens to the test laboratory at least 3 h before the tests.

After cleaning and equilibration, the samples need to be broken with a pendulum impact test machine operated in accordance with EN 10045-1 or ISO 148-1 standards. Prior to the tests, the anvils must be cleaned. It must be noted that Charpy test pieces sometimes leave debris on the Charpy pendulum anvils. Therefore, the anvils must be checked regularly and if debris is found, it must be removed.

For some pendulums and for some samples, post-fracture interaction between broken samples and pendulum hammer can affect the measured KV values. The resulting excessively high values can be related to indentations and deformations of the broken samples. Outlier values that can be related to post-fracture indentation marks on the broken samples must be eliminated from the analysis of the results.

## STORAGE

Specimens should be kept at room temperature in their original packing until used. However, the European Commission cannot be held responsible for changes that happen during storage of the material at the customer's premises, especially of opened samples.

## LEGAL NOTICE

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## NOTE

A detailed technical report can be obtained from the Joint Research Centre, Institute for Reference Materials and Measurements on request.

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European Commission – Joint Research Centre  
Institute for Reference Materials and Measurements (IRMM)  
Retieseweg 111, B - 2440 Geel (Belgium)  
Telephone: +32-(0)14-571.722 - Fax: +32-(0)14-590.406

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# CERTIFICATE OF ANALYSIS

ERM<sup>®</sup> - FA013ay

STEEL		
	Impact toughness at 0 °C	
	Certified value <sup>2)</sup> [J]	Uncertainty <sup>3)</sup> [J]
Absorbed energy (KV) <sup>1)</sup>	26.06	0.35
<p>1) The absorbed energy (KV) is procedurally defined and refers to the impact energy required to break a V-notched bar of standardised dimensions, as defined in EN 10045-1 and ISO 148-1.</p> <p>2) The certified value is estimated as the mean of means of absorbed energies measured at 12 laboratories. At each laboratory, 20 test pieces were broken. The instruments used by these laboratories are regularly verified with equipment that is calibrated in a manner that is traceable to the International System of Units (SI). Therefore, the certified value is traceable to the International System of Units (SI).</p> <p>3) Standard uncertainty <i>u</i> of the certified mean absorbed energy of batch ERM-FA013ay, estimated as the standard deviation of the mean of the 12 laboratory mean values, corresponding with a confidence level of about 68 %.</p>		

This certificate is valid until November 2018.

## NOTE

European Reference Material ERM<sup>®</sup>-FA013ay was produced and certified under the responsibility of the Institute for Reference Materials and Measurements of the European Commission's Joint Research Centre according to the principles laid down in the technical guidelines of the European Reference Materials<sup>®</sup> co-operation agreement between BAM-IRMM-LGC. Information on these guidelines is available on the internet (<http://www.erm-crm.org>).

Accepted as an ERM<sup>®</sup>, Geel, July 2011

Signed: \_\_\_\_\_



Prof. Dr. Hendrik Emons  
European Commission  
Joint Research Centre  
Institute for Reference Materials and Measurements  
Retieseweg 111  
B-2440 Geel, Belgium



Registration No. 268-TEST  
ISO Guide 34 for the  
production of reference materials

All following pages are an integral part of the certificate.

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## DESCRIPTION OF THE SAMPLE

A unit consists of five Charpy V-notch test pieces, which are rectangular steel bars of nominal dimensions 55 mm x 10 mm x 10 mm, with one V-notch, accurately machined to tolerances imposed in EN 10045-2 and ISO 148-3. The five specimens are packed together in a plastic bag filled with oil to prevent oxidation.

## ANALYTICAL METHOD USED FOR CERTIFICATION

Charpy pendulum impact tests in accordance with EN 10045-1 and ISO 148-1, using pendulum impact machines with a 2 mm striker tip radius.

## PARTICIPANTS

- Aubert&Duval, Les Ancizes and Gennevilliers (FR)
- Bodycote Materials Testing (now Exova), Emmen (NL)\* (RvA testen L085)
- Bodycote Materials Testing (now Exova), Spijkenisse (NL)\* (RvA testen L085)
- Bundesanstalt für Materialforschung und -prüfung (BAM), Abteilung V Werkstofftechnik, Berlin (DE)\* (DAP-PL-2614.16)
- Centro de Apoio Tecnológico a Industria Metalomechanica (CATIM), Laboratório de Ensaios, Porto (PT)\* (IPAC L009)
- Cogne Acciai Speciali, Aosta (IT)
- Fraunhofer Gesellschaft, Institut für Werkstoffmechanik, Freiburg (DE)
- European Commission Joint Research Centre (JRC), Institute for Reference Materials and Measurements, Geel (BE) (BELAC 268-Test)
- Laboratoire National de Métrologie et d'Essais, Charpy Laboratory, Trappes (FR)\* (COFRAC SMH 2-1287)
- SCK-CEN, Labo Reactormaterialenonderzoek, Mol (BE)\* (BELAC 015-Test)
- SIRRIS, Beproevinglaboratorium Gent, Zwijnaarde (BE)\* (BELAC 232-Test)
- U.S. Steel Košice, Labortest, Košice (SK)\* (SNAS 026/S012)
- Universität Stuttgart, Materialprüfungsanstalt, Stuttgart (DE)\* (DAP-PL-2907.02)

\* Measurements within the scope of accreditation to ISO 17025.

## SAFETY INFORMATION

Precautions need to be taken to avoid injury of the operator by broken specimens when operating the Charpy impact pendulum.

## INSTRUCTIONS FOR USE

Samples of ERM-FA013ay correspond with the '(certified) BCR test pieces' as referred to in EN 10045-2 (Method for the verification of impact testing machines), as well as with the 'certified reference test pieces' as defined in ISO 148-3 (Preparation and characterisation of Charpy V reference test pieces for verification of test machines).

The ERM-FA013ay batch is one of the 'Master Batches'. Master Batch test pieces are not for sale. They are intended solely to traceably certify Secondary Batches of the same nominal absorbed energy (here 30 J). The certified value and its associated uncertainty of the Master Batch are used in the calculation of the certified value and combined and expanded uncertainty of a set of 5 specimens from a Secondary Batch. Because the certified value of the Master Batch, and its uncertainty, are intermediate values, they have not been rounded according to normal rounding procedures. Instead one additional digit is preserved.

When characterising a secondary batch, a number of Master Batch test pieces are broken under repeatability conditions together with a selection of samples from the secondary batch. Special attention is drawn to the cleaning and conditioning of the specimens prior to testing. It is mandatory to remove the oil from the sample surface prior to testing, without damaging the edges of the sample. Between the moment of removing the protective oil layer and the actual test, corrosion can occur. This must be avoided by limiting this period of time, while keeping the sample clean.



The following cleaning and conditioning procedure is considered to be good practice.

1. First use absorbent cleaning-tissue to remove the excess oil. Pay particular attention to the notch of the sample, but do not use hard (e.g. steel) brushes to remove the oil from the notch.
2. Submerge the samples in technically pure ethanol for about 5 minutes. Use of ultrasonication is encouraged, but only if the edges of the samples are prevented from rubbing against each other. To reduce the consumption of solvent, it is allowed to make a first cleaning step with detergent, immediately prior to the solvent step.
3. Once samples are removed from the solvent, only manipulate the samples wearing clean gloves. This is to prevent development of corrosion between the time of cleaning and the actual test.
4. Before testing, bring the specimens to the test temperature ( $0 \pm 2$  °C). To assure thermal equilibrium, the specimens shall be at least 10 minutes in a liquid cooling medium or at least 30 minutes in a gaseous cooling medium, the temperature of which is measured and monitored. The test piece shall be broken within 5 seconds of the time of removal from the cooling medium.

After cleaning and equilibration, the samples need to be broken with a pendulum impact test machine operated in accordance with EN 10045-1 or ISO 148-1 standards. Prior to the tests, the anvils must be cleaned. It must be noted that Charpy test pieces sometimes leave debris on the Charpy pendulum anvils. Therefore, the anvils must be checked regularly and if debris is found, it must be removed.

For some pendulums and for some samples, post-fracture interaction between broken samples and pendulum hammer can affect the measured KV values. The resulting excessively high values can be due to indentations and deformations of the broken samples. Outlier values that can be related to post-fracture indentation marks on the broken samples must be eliminated from the analysis of the results.

## STORAGE

Specimens should be kept at room temperature in their original packing until used. However, the European Commission cannot be held responsible for changes that happen during storage of the material at the customer's premises, especially of opened samples.

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## NOTE

A detailed technical report can be obtained from the Joint Research Centre, Institute for Reference Materials and Measurements on request.

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European Commission – Joint Research Centre  
Institute for Reference Materials and Measurements (IRMM)  
Retieseweg 111, B - 2440 Geel (Belgium)  
Telephone: +32-(0)14-571.722 - Fax: +32-(0)14-590.406

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European Commission

**EUR 25840 EN – Joint Research Centre – Institute for Reference Materials and Measurements**

Title: The certification of the absorbed energy (30 J nominal) of Charpy V-notch reference test pieces for tests at 20 °C and at 0 °C: ERM<sup>®</sup>-FA013bk

Author(s): A. Lamberty, A. Dean, G. Roebben

European Commission, Joint Research Centre

Institute for Reference Materials and Measurements (IRMM) Geel, Belgium

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**Abstract**

This certification report describes the processing and characterisation of ERM<sup>®</sup>-FA013bk, a batch of Charpy V-notch certified reference test pieces certified for the absorbed energy (KV) for tests at 20 °C and at 0 °C. Sets of five of these test pieces are used for the verification of pendulum impact test machines according to ISO 148-2 (Metallic materials - Charpy pendulum impact test – Part 2: Verification of testing machines [1]).

The absorbed energy (KV) is procedurally defined and refers to the impact energy required to break a V-notched test piece of standardised dimensions, as defined in ISO 148-1 [2]. The certified value of ERM-FA013bk is traceable to the SI, via the SI-traceable certified value of the master batches ERM-FA013ba and ERM-FA013ay, by testing samples of ERM-FA013bk and ERM-FA013ba and ERM-FA013bk and ERM-FA013ay respectively, under repeatability conditions on an impact pendulum verified and calibrated with SI-traceably calibrated tools. The certified value is valid only for strikers with a 2 mm tip radius. The certified values are valid at  $(20 \pm 2)$  °C and  $(0 \pm 2)$  °C respectively.

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